



## Supporting Online Material for

### Rapid Glacial Erosion at 1.8 Ma Revealed by $^4\text{He}/^3\text{He}$ Thermochronometry

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Published 9 December 2005, *Science* **310**, p1668 (2005)  
DOI: 10.1126/science.1118519

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**Supplementary Information for:**

**Shuster, D.L., T.A. Ehlers, M.E. Rusmore, and K.A. Farley (2005)**

**Rapid Glacial Erosion at 1.8 Ma Revealed by  $^4\text{He}/^3\text{He}$  Thermochronometry, *Science***

Thermochronometry often involves the determination of a cooling age from parent and daughter abundances within an entire crystal or population of crystals (1). Complementary information exists in the spatial concentration distribution of the daughter within a single crystal. By combining a bulk cooling age with the spatial distribution of the daughter on the same sample, it is possible to place tight limits on the sample's time-temperature ( $t$ - $T$ ) path

This approach is applied to the (U-Th)/He system by introducing synthetic  $^3\text{He}$  via proton irradiation (2). The attraction of the (U-Th)/He system is its sensitivity to uniquely low temperatures. For example, the nominal  $^4\text{He}$  closure temperature (at  $10^\circ\text{C}/\text{Myr}$ ) for apatite is  $60^\circ\text{C}$  (3). Therefore, significant diffusion of  $^4\text{He}$  occurs at temperatures just slightly higher than those of Earth's surface.

In  $^4\text{He}/^3\text{He}$  thermochronometry (4), the natural spatial distribution of  $^4\text{He}$  is constrained by stepwise degassing  $^4\text{He}/^3\text{He}$  analysis of a sample containing synthetic, proton-induced  $^3\text{He}$ . Since the distribution of the  $^3\text{He}$  is spatially uniform (2), release fractions of proton-induced  $^3\text{He}$  can be used to determine the helium diffusion kinetics (5) (e.g., Fig. S1-S4, panels (a)). Upon stepwise degassing, sequentially measured  $^4\text{He}/^3\text{He}$  ratios constrain the natural  $^4\text{He}$  distribution within an individual crystal or a small population of crystals. Evolution of the  $^4\text{He}/^3\text{He}$  ratio reveals the distribution of radiogenic  $^4\text{He}$  within a sample. For instance, a  $^4\text{He}$  distribution solely resulting from  $\alpha$ -ejection (6) (i.e., due to rapid cooling), will have relatively high  $^4\text{He}/^3\text{He}$  ratios at the beginning of a degassing experiment. Conversely, a diffusive  $^4\text{He}$  distribution resulting from gradual cooling will have low  $^4\text{He}$  near the grain's edge and therefore low initial  $^4\text{He}/^3\text{He}$  ratios which steadily rise over the course of an analysis (4). The  $^4\text{He}/^3\text{He}$  ratios of the first ~40% of helium extracted over the course of an analysis contain the highest resolving power on the  $^4\text{He}$  distribution (4). Note that the  $^4\text{He}/^3\text{He}$  ratios measured toward the end of an experiment are often not useful for constraining the spatial distribution of  $^4\text{He}$  in the sample, but must be incorporated when calculating the bulk  $^4\text{He}/^3\text{He}$  ratio of a sample (7).

Together, the helium diffusion kinetics and the spatial distribution of  $^4\text{He}$  can be used to constrain the sample's  $t$ - $T$  path. To quantify a sample's thermal history from an observed radiometric age and an inferred spatial distribution of the daughter product is formally an ill posed problem: a set of  $t$ - $T$  solutions can be constrained, although a single solution does not generally exist. The age and concentration profile together limit acceptable cooling paths.

As discussed in the main text, the  $^4\text{He}/^3\text{He}$  results of 01MR-59 demand rapid cooling of at least  $50^\circ\text{C}$  at between 1.8 Ma and 1.4 Ma. A cooling event of this magnitude should be recorded in proximate samples. Here, we use the  $^4\text{He}/^3\text{He}$  results for samples (TEKI-38, TEKI-34, TEKI-30, and TEKI-23) collected along a nearly vertical profile to test this cooling model. The models presented below are an internally consistent set of solutions that have been bootstrapped from the 01MR-59 result. All models were constrained to a vertical geothermal gradient  $\leq 30^\circ\text{C}/\text{km}$ . From this analysis, we find that all samples at elevation  $\leq 2000$  m support the occurrence of a rapid

cooling event at  $1.8 \pm 0.2$  Ma. Together, the set of solutions places tight constraints on the thermal history of the valley.

**Tables S1-S5**  $^4\text{He}/^3\text{He}$  thermochronometry data tables for TEKI-38 (**S1**), TEKI-34 (**S2**), TEKI-30 (**S3**) and TEKI-23 (**S4**), and 01MR-59 (**S5**), respectively.

**Figures S1-S5**  $^4\text{He}/^3\text{He}$  thermochronometry for apatite samples TEKI-38 (**S1**), TEKI-34 (**S2**), TEKI-30 (**S3**), TEKI-23 (**S4**) and 01MR-59 (**S5**), respectively. **(a)** Arrhenius plots; circles are the diffusion coefficients,  $D$ , normalized to the diffusive length scale,  $a$ , calculated (5) from release fractions of proton-induced  $^3\text{He}$  (2). Solid black line is the inferred helium diffusion kinetics for each sample used to construct models shown in (b,c), determined by linear regression of a subset array. Steps deviate from linearity above  $300^\circ\text{C}$  due to a change in mechanism (3) which may not apply to lower temperatures relevant to our models and are therefore excluded from the regression. **(b)** Model  $t$ - $T$  paths. Each of these models corresponds to the observed (U-Th)/He age for each sample, which is indicated in the lower panels. **(c)** Ratio evolution diagrams. Shown are measured isotope ratios for each release step,  $R_{\text{step}}$  ( $R = ^4\text{He}/^3\text{He}$ ), normalized to the bulk ratio  $R_{\text{bulk}}$ , plotted versus the cumulative  $^3\text{He}$  release fraction,  $\Sigma F^3\text{He}$ . Each model shown in (c) corresponds to the  $t$ - $T$  path in (b). Also shown for reference are two end-member  $^4\text{He}$  distributions, i.e., the  $\alpha$ -ejection only distribution (dashed line) and the steady-state distribution (dotted line) (4). Due to a change in diffusive mechanism at temperatures  $>300^\circ\text{C}$  which were used toward the end of these experiments (3), and because the initially extracted gas contains the highest resolving power on the spatial distribution of  $^4\text{He}$  (4), models were matched only to values of  $\Sigma F^3\text{He} \leq 0.4$ . For these reasons, data collected for  $\Sigma F^3\text{He} > 0.6$  do not well represent the spatial distribution of  $^4\text{He}$  (7) and were not considered in our modeling, although all points were used to calculate the bulk  $^4\text{He}/^3\text{He}$  ratio of each sample. Error bars are specified by a vertical line through each point. Data scatter and uncertainty is largely a function of the absolute  $^4\text{He}$  abundance in each sample and the corresponding magnitude of  $^4\text{He}$  blank corrections. For instance, TEKI-38 contains a  $^4\text{He}$  abundance that is 7% of that of TEKI-23.

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Table S1: TEKI-38

| Step  | T (oC) | time (hr) | <sup>3</sup> He<br>(atoms/10 <sup>6</sup> ) | $R_{\text{step}}/R_{\text{bulk}}^*$ | (+/-) |
|-------|--------|-----------|---|-------------------------------------|-------|
| 1     | 150    | 0.50      | 0.09  | b.d.                                | b.d.  |
| 2     | 150    | 0.75      | 0.06  | b.d.                                | b.d.  |
| 3     | 150    | 1.00      | 0.05  | b.d.                                | b.d.  |
| 4     | 175    | 0.75      | 0.16  | b.d.                                | b.d.  |
| 5     | 175    | 1.25      | 0.18  | b.d.                                | b.d.  |
| 6     | 200    | 0.75      | 0.40  | b.d.                                | b.d.  |
| 7     | 200    | 1.25      | 0.46  | b.d.                                | b.d.  |
| 8     | 225    | 0.50      | 0.60  | 0.29                                | 0.47  |
| 9     | 225    | 1.25      | 1.09  | 0.42                                | 0.27  |
| 10    | 250    | 0.75      | 1.74  | 0.27                                | 0.17  |
| 11    | 250    | 1.25      | 1.81  | 0.58                                | 0.16  |
| 12    | 240    | 1.25      | 0.97  | 0.53                                | 0.30  |
| 13    | 230    | 1.50      | 0.58  | b.d.                                | b.d.  |
| 14    | 220    | 2.00      | 0.35  | b.d.                                | b.d.  |
| 15    | 235    | 2.50      | 0.89  | b.d.                                | b.d.  |
| 16    | 275    | 0.75      | 2.48  | 0.38                                | 0.12  |
| 17    | 275    | 1.25      | 2.55  | 0.59                                | 0.12  |
| 18    | 300    | 0.75      | 3.91  | 0.50                                | 0.08  |
| 19    | 300    | 1.25      | 4.63  | 0.68                                | 0.07  |
| 20    | 325    | 0.50      | 4.57  | 0.55                                | 0.07  |
| 21    | 325    | 1.25      | 8.44  | 0.69                                | 0.05  |
| 22    | 350    | 1.25      | 13.15                                       | 0.87                                | 0.03  |
| 23    | 375    | 0.50      | 10.37                                       | 0.81                                | 0.04  |
| 24    | 425    | 0.50      | 22.84                                       | 1.03                                | 0.02  |
| 25    | 475    | 0.50      | 29.55                                       | 1.15                                | 0.02  |
| 26    | 525    | 0.50      | 21.76                                       | 1.26                                | 0.03  |
| 27    | 575    | 0.50      | 5.81  | 1.51                                | 0.06  |
| 28    | 600    | 0.50      | 1.37  | 1.92                                | 0.22  |
| 29    | 600    | 1.00      | 0.49  | 3.68                                | 0.59  |
| 30    | 600    | 2.00      | 0.15  | 9.66                                | 1.94  |
| 31    | 1200   | 0.10      | 0.86  | 1.73                                | 0.27  |
| Total |        |           | 142.36                                      |                                     |       |

\* $R = {}^4\text{He}/{}^3\text{He}$ ,  $R_{\text{bulk}} = 26$

b.d. is below detection limit

Table S2: TEKI-34

| Step  | T (oC) | time (hr) | <sup>3</sup> He<br>(atoms/10 <sup>6</sup> ) | $R_{\text{step}}/R_{\text{bulk}}^*$ | (+/-) |
|-------|--------|-----------|---|-------------------------------------|-------|
| 1     | 150    | 0.50      | 0.12  | b.d                                 | b.d   |
| 2     | 150    | 0.75      | 0.08  | b.d                                 | b.d   |
| 3     | 150    | 1.00      | 0.07  | b.d                                 | b.d   |
| 4     | 175    | 0.75      | 0.24  | b.d                                 | b.d   |
| 5     | 175    | 1.25      | 0.27  | 0.37                                | 0.80  |
| 6     | 200    | 0.75      | 0.64  | 0.10                                | 0.34  |
| 7     | 200    | 1.25      | 0.72  | 0.25                                | 0.30  |
| 8     | 225    | 0.50      | 0.83  | 0.26                                | 0.27  |
| 9     | 225    | 1.25      | 1.61  | 0.47                                | 0.14  |
| 10    | 250    | 0.75      | 3.32  | 0.36                                | 0.07  |
| 11    | 250    | 1.25      | 3.74  | 0.52                                | 0.07  |
| 12    | 240    | 1.25      | 1.90  | 0.49                                | 0.12  |
| 13    | 230    | 1.50      | 0.88  | 0.46                                | 0.25  |
| 14    | 220    | 2.00      | 0.61  | 0.46                                | 0.37  |
| 15    | 235    | 2.50      | 1.72  | 0.49                                | 0.14  |
| 16    | 275    | 0.75      | 6.03  | 0.57                                | 0.05  |
| 17    | 275    | 1.25      | 6.18  | 0.63                                | 0.05  |
| 18    | 300    | 0.75      | 9.10  | 0.67                                | 0.03  |
| 19    | 300    | 1.25      | 6.32  | 0.73                                | 0.04  |
| 20    | 325    | 0.50      | 5.70  | 0.69                                | 0.05  |
| 21    | 325    | 1.25      | 10.56                                       | 0.79                                | 0.03  |
| 22    | 350    | 1.25      | 18.14                                       | 0.86                                | 0.02  |
| 23    | 375    | 0.50      | 12.58                                       | 0.97                                | 0.03  |
| 24    | 425    | 0.50      | 36.59                                       | 1.01                                | 0.02  |
| 25    | 475    | 0.50      | 57.06                                       | 1.10                                | 0.01  |
| 26    | 525    | 0.50      | 53.67                                       | 1.21                                | 0.01  |
| 27    | 575    | 0.50      | 21.78                                       | 1.23                                | 0.02  |
| 28    | 600    | 0.50      | 3.31  | 1.65                                | 0.07  |
| 29    | 600    | 1.00      | 1.29  | 2.14                                | 0.17  |
| 30    | 600    | 2.00      | 1.13  | 2.44                                | 0.19  |
| 31    | 1200   | 0.10      | 2.99  | 0.45                                | 0.09  |
| Total |        |           | 269.21                                      |                                     |       |

\* $R = {}^4\text{He}/{}^3\text{He}$ ,  $R_{\text{bulk}} = 52$

b.d. is below detection limit

Table S3: TEKI-30

| Step  | T (oC) | time (hr) | <sup>3</sup> He<br>(atoms/10 <sup>6</sup> ) | $R_{\text{step}}/R_{\text{bulk}}^*$ | (+/-) |
|-------|--------|-----------|---|-------------------------------------|-------|
| 1     | 150    | 0.50      | 0.08  | b.d.                                | b.d.  |
| 2     | 150    | 0.75      | 0.04  | b.d.                                | b.d.  |
| 3     | 150    | 1.00      | 0.06  | b.d.                                | b.d.  |
| 4     | 175    | 0.75      | 0.14  | b.d.                                | b.d.  |
| 5     | 175    | 1.25      | 0.15  | b.d.                                | b.d.  |
| 6     | 200    | 0.75      | 0.35  | 0.18                                | 0.64  |
| 7     | 200    | 1.25      | 0.36  | 0.22                                | 0.63  |
| 8     | 225    | 0.50      | 0.50  | 0.19                                | 0.46  |
| 9     | 225    | 1.25      | 0.84  | 0.34                                | 0.29  |
| 10    | 250    | 0.75      | 1.53  | 0.38                                | 0.17  |
| 11    | 250    | 1.25      | 1.63  | 0.43                                | 0.16  |
| 12    | 240    | 1.25      | 0.67  | 0.38                                | 0.36  |
| 13    | 230    | 1.50      | 0.47  | 0.42                                | 0.50  |
| 14    | 220    | 2.00      | 0.32  | 0.26                                | 0.73  |
| 15    | 235    | 2.50      | 0.76  | 0.58                                | 0.32  |
| 16    | 275    | 0.75      | 1.65  | 0.45                                | 0.15  |
| 17    | 275    | 1.25      | 2.31  | 0.61                                | 0.11  |
| 18    | 300    | 0.75      | 3.31  | 0.64                                | 0.08  |
| 19    | 300    | 1.25      | 4.29  | 0.71                                | 0.06  |
| 20    | 325    | 0.50      | 3.59  | 0.71                                | 0.07  |
| 21    | 325    | 1.25      | 6.87  | 0.86                                | 0.04  |
| 22    | 350    | 1.25      | 11.87                                       | 0.91                                | 0.03  |
| 23    | 375    | 0.50      | 7.95  | 0.93                                | 0.04  |
| 24    | 425    | 0.50      | 22.34                                       | 1.06                                | 0.02  |
| 25    | 475    | 0.50      | 30.99                                       | 1.19                                | 0.02  |
| 26    | 525    | 0.50      | 26.62                                       | 1.15                                | 0.02  |
| 27    | 575    | 0.50      | 8.58  | 1.13                                | 0.04  |
| 28    | 600    | 0.50      | 1.16  | 1.36                                | 0.22  |
| 29    | 600    | 1.00      | 0.77  | 1.45                                | 0.32  |
| 30    | 600    | 2.00      | 0.55  | 2.16                                | 0.45  |
| 31    | 1200   | 0.10      | 1.63  | 1.21                                | 0.06  |
| Total |        |           | 142.38                                      |                                     |       |

\* $R = {}^4\text{He}/{}^3\text{He}$ ,  $R_{\text{bulk}} = 96$

b.d. is below detection limit

Table S4: TEKI-23

| Step  | T (oC) | time (hr) | <sup>3</sup> He<br>(atoms/10 <sup>6</sup> ) | $R_{\text{step}}/R_{\text{bulk}}^*$ | (+/-) |
|-------|--------|-----------|---|-------------------------------------|-------|
| 1     | 150    | 0.50      | 0.10  | b.d.                                | b.d.  |
| 2     | 150    | 0.75      | 0.10  | b.d.                                | b.d.  |
| 3     | 150    | 1.00      | 0.19  | b.d.                                | b.d.  |
| 4     | 175    | 0.75      | 0.38  | b.d.                                | b.d.  |
| 5     | 175    | 1.25      | 0.39  | b.d.                                | b.d.  |
| 6     | 200    | 0.75      | 0.83  | b.d.                                | b.d.  |
| 7     | 200    | 1.25      | 0.88  | 0.35                                | 0.16  |
| 8     | 225    | 0.50      | 1.26  | 0.34                                | 0.12  |
| 9     | 225    | 1.25      | 2.15  | 0.38                                | 0.07  |
| 10    | 250    | 0.75      | 2.92  | 0.45                                | 0.05  |
| 11    | 250    | 1.25      | 3.61  | 0.49                                | 0.04  |
| 12    | 240    | 1.25      | 1.65  | 0.54                                | 0.09  |
| 13    | 230    | 1.50      | 1.05  | 0.55                                | 0.15  |
| 14    | 220    | 2.00      | 0.81  | 0.51                                | 0.19  |
| 15    | 235    | 2.50      | 1.95  | 0.59                                | 0.08  |
| 16    | 275    | 0.75      | 3.48  | 0.56                                | 0.05  |
| 17    | 275    | 1.25      | 4.45  | 0.61                                | 0.04  |
| 18    | 300    | 0.75      | 6.70  | 0.64                                | 0.03  |
| 19    | 300    | 1.25      | 7.47  | 0.71                                | 0.03  |
| 20    | 325    | 0.50      | 5.97  | 0.75                                | 0.03  |
| 21    | 325    | 1.25      | 11.01                                       | 0.78                                | 0.02  |
| 22    | 350    | 1.25      | 18.16                                       | 0.89                                | 0.02  |
| 23    | 375    | 0.50      | 10.38                                       | 0.96                                | 0.02  |
| 24    | 425    | 0.50      | 28.16                                       | 1.02                                | 0.01  |
| 25    | 475    | 0.50      | 36.15                                       | 1.12                                | 0.01  |
| 26    | 525    | 0.50      | 28.21                                       | 1.17                                | 0.01  |
| 27    | 575    | 0.50      | 17.64                                       | 1.14                                | 0.01  |
| 28    | 600    | 0.50      | 9.52  | 1.13                                | 0.02  |
| 29    | 600    | 1.00      | 7.68  | 1.13                                | 0.03  |
| 30    | 600    | 2.00      | 5.24  | 1.36                                | 0.02  |
| 31    | 1200   | 0.10      | 6.56  | 1.35                                | 0.02  |
| Total |        |           | 225.04                                      |                                     |       |

\* $R = {}^4\text{He}/{}^3\text{He}$ ,  $R_{\text{bulk}} = 356$

b.d. is below detection limit

Table S5: Apatite 01mr-59

| Step  | T (oC) | time (hr) | <sup>3</sup> He<br>(atoms/10 <sup>6</sup> ) | $R_{\text{step}}/R_{\text{bulk}}^*$ | (+/-) |
|-------|--------|-----------|---|-------------------------------------|-------|
| 1     | 175    | 0.75      | 0.35  | 0.134                               | 0.051 |
| 2     | 175    | 1.00      | 0.17  | 0.183                               | 0.076 |
| 3     | 175    | 3.00      | 0.21  | 0.345                               | 0.127 |
| 4     | 188    | 1.00      | 0.13  | 0.458                               | 0.165 |
| 5     | 188    | 1.50      | 0.17  | 0.423                               | 0.147 |
| 6     | 188    | 2.00      | 0.16  | 0.268                               | 0.108 |
| 7     | 200    | 0.50      | 0.08  | 0.275                               | 0.118 |
| 8     | 200    | 1.00      | 0.16  | 0.368                               | 0.134 |
| 9     | 200    | 1.50      | 0.22  | 0.379                               | 0.126 |
| 10    | 200    | 2.00      | 0.27  | 0.563                               | 0.153 |
| 11    | 225    | 0.50      | 0.32  | 0.663                               | 0.135 |
| 12    | 225    | 2.00      | 0.80  | 0.537                               | 0.080 |
| 13    | 225    | 2.00      | 0.73  | 0.551                               | 0.086 |
| 14    | 250    | 0.50      | 0.69  | 0.724                               | 0.082 |
| 15    | 250    | 1.00      | 1.09  | 0.562                               | 0.057 |
| 16    | 250    | 2.00      | 1.51  | 0.580                               | 0.050 |
| 17    | 275    | 0.50      | 1.22  | 0.615                               | 0.050 |
| 18    | 275    | 1.00      | 1.97  | 0.671                               | 0.036 |
| 19    | 275    | 2.00      | 2.87  | 0.682                               | 0.029 |
| 20    | 295    | 0.50      | 1.53  | 0.691                               | 0.042 |
| 21    | 295    | 1.00      | 2.52  | 0.732                               | 0.029 |
| 22    | 295    | 2.00      | 3.80  | 1.003                               | 0.023 |
| 23    | 305    | 0.50      | 1.15  | 0.819                               | 0.054 |
| 24    | 305    | 1.00      | 2.23  | 0.802                               | 0.032 |
| 25    | 305    | 1.25      | 2.30  | 0.805                               | 0.033 |
| 26    | 305    | 2.00      | 3.00  | 0.834                               | 0.028 |
| 27    | 315    | 0.50      | 1.04  | 0.877                               | 0.060 |
| 28    | 315    | 1.00      | 1.91  | 0.874                               | 0.038 |
| 29    | 315    | 1.25      | 1.89  | 0.912                               | 0.039 |
| 30    | 315    | 1.75      | 2.56  | 0.908                               | 0.032 |
| 31    | 325    | 0.50      | 1.01  | 0.928                               | 0.062 |
| 32    | 325    | 1.50      | 2.15  | 0.981                               | 0.036 |
| 33    | 325    | 1.50      | 2.14  | 0.947                               | 0.036 |
| 34    | 325    | 2.00      | 2.30  | 0.970                               | 0.036 |
| 35    | 335    | 0.50      | 0.87  | 0.971                               | 0.071 |
| 36    | 335    | 1.00      | 1.57  | 0.979                               | 0.066 |
| 37    | 335    | 1.50      | 2.00  | 1.044                               | 0.073 |
| 38    | 335    | 2.00      | 2.41  | 1.121                               | 0.078 |
| 39    | 345    | 1.00      | 1.69  | 1.048                               | 0.082 |
| 40    | 350    | 0.50      | 1.00  | 1.003                               | 0.094 |
| 41    | 360    | 0.50      | 1.39  | 0.973                               | 0.071 |
| 42    | 360    | 1.00      | 2.16  | 1.044                               | 0.034 |
| 43    | 370    | 0.50      | 1.58  | 1.000                               | 0.042 |
| 44    | 370    | 1.00      | 2.46  | 1.026                               | 0.030 |
| 45    | 380    | 0.50      | 1.43  | 1.052                               | 0.046 |
| 46    | 390    | 0.50      | 1.73  | 1.067                               | 0.039 |
| 47    | 400    | 1.00      | 3.14  | 1.307                               | 0.076 |
| 48    | 425    | 0.50      | 2.80  | 1.127                               | 0.025 |
| 49    | 450    | 0.25      | 2.07  | 1.185                               | 0.032 |
| 50    | 450    | 0.25      | 1.94  | 1.111                               | 0.034 |
| 51    | 475    | 0.25      | 2.37  | 1.120                               | 0.028 |
| 52    | 475    | 0.25      | 1.46  | 1.151                               | 0.044 |
| 53    | 475    | 0.50      | 1.61  | 1.362                               | 0.042 |
| 54    | 475    | 0.50      | 0.89  | 1.445                               | 0.073 |
| 55    | 500    | 0.25      | 0.62  | 1.467                               | 0.097 |
| 56    | 500    | 0.25      | 0.34  | 1.593                               | 0.162 |
| 57    | 550    | 0.50      | 0.71  | 1.693                               | 0.156 |
| 58    | 550    | 0.75      | 0.45  | 2.602                               | 0.363 |
| 59    | 550    | 1.00      | 0.43  | 1.895                               | 0.339 |
| 60    | 550    | 3.00      | 0.47  | 1.538                               | 0.317 |
| 61    | 525    | 5.00      | 0.72  | 1.619                               | 0.260 |
| 62    | 525    | 5.00      | 0.62  | 1.330                               | 0.268 |
| 63    | 600    | 5.00      | 0.97  | 1.535                               | 0.208 |
| 64    | 600    | 5.00      | 0.88  | 1.615                               | 0.228 |
| 65    | 620    | 5.00      | 0.72  | 1.663                               | 0.263 |
| 66    | 1200   | 0.10      | 1.74  | 1.660                               | 0.271 |
| Total |        |           | 89.89                                       |                                     |       |

\* $R = {}^4\text{He}/{}^3\text{He}$ ,  $R_{\text{bulk}} = 236$











